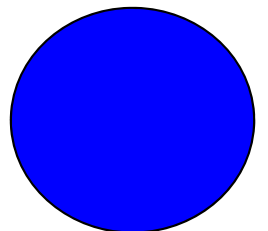


# Active media and unstable filters: Commonalities and difference

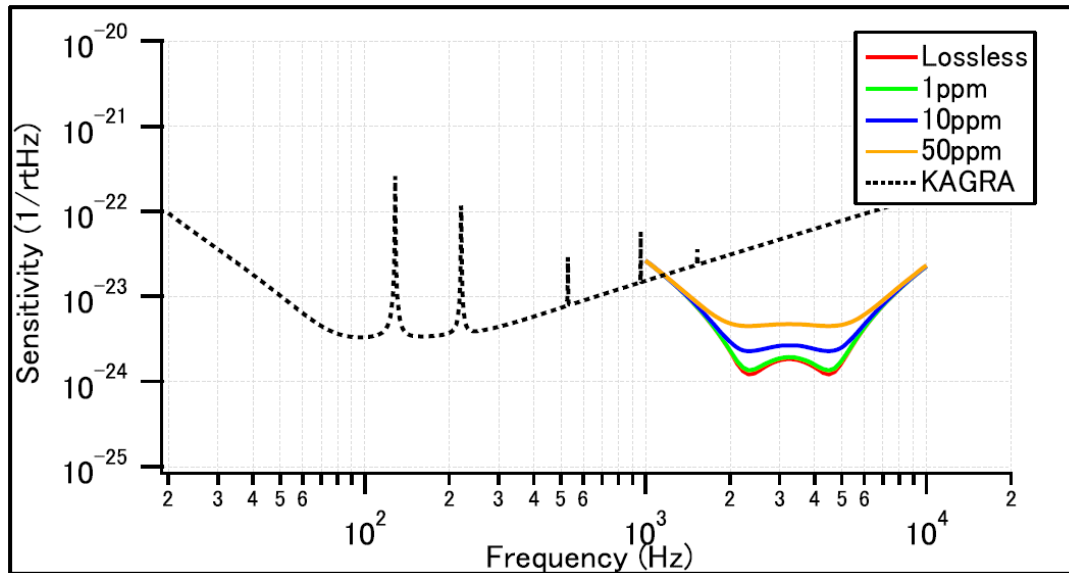
GWADW  
May 2018

K.Somiya  
(also presenting slides by H.Miao)

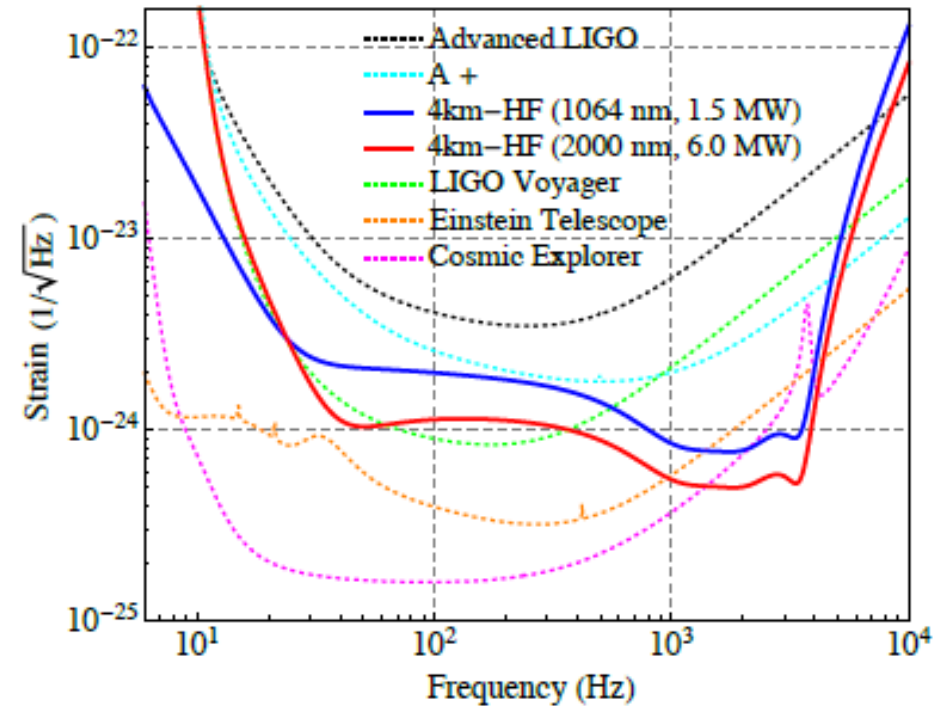


K.Somiya

# Introduction



My plot for GEO-HF upgrade.



Haixing's plot for aLIGO upgrade.

**Both are with an active device in the SR cavity.**

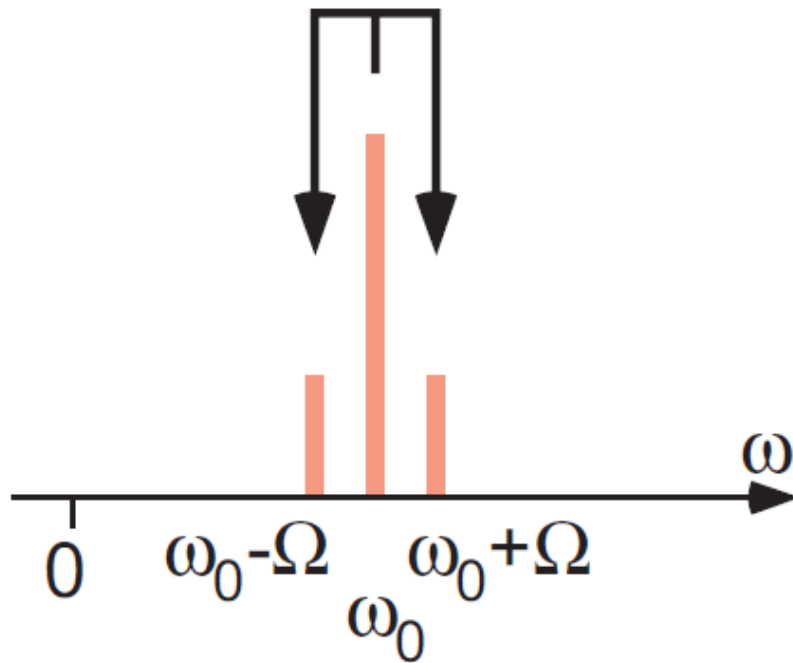
**I will show you,**

**(i) Commonality of the schemes**

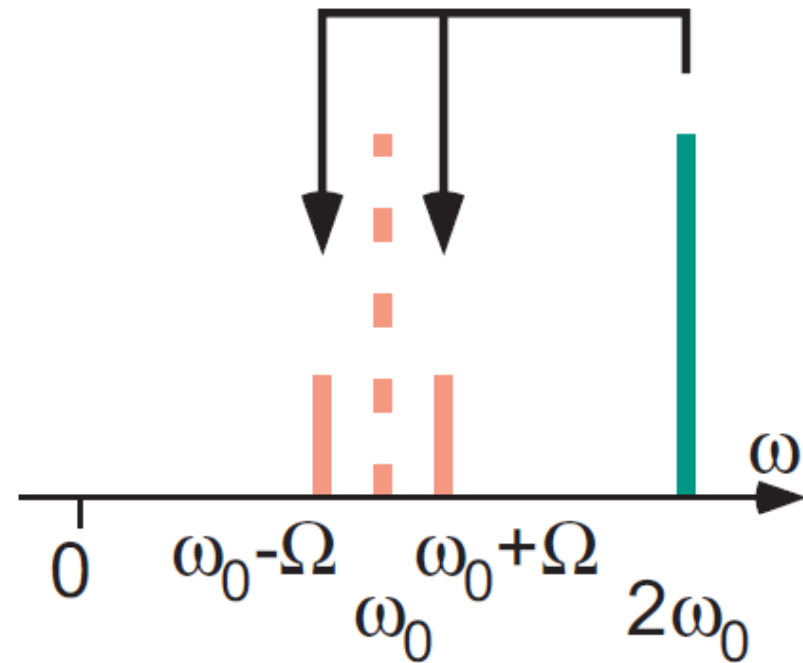
**(ii) Current status of Haixing's scheme**

**(iii) Current status of Our scheme.**

# Ponderomotive and OPO squeezings

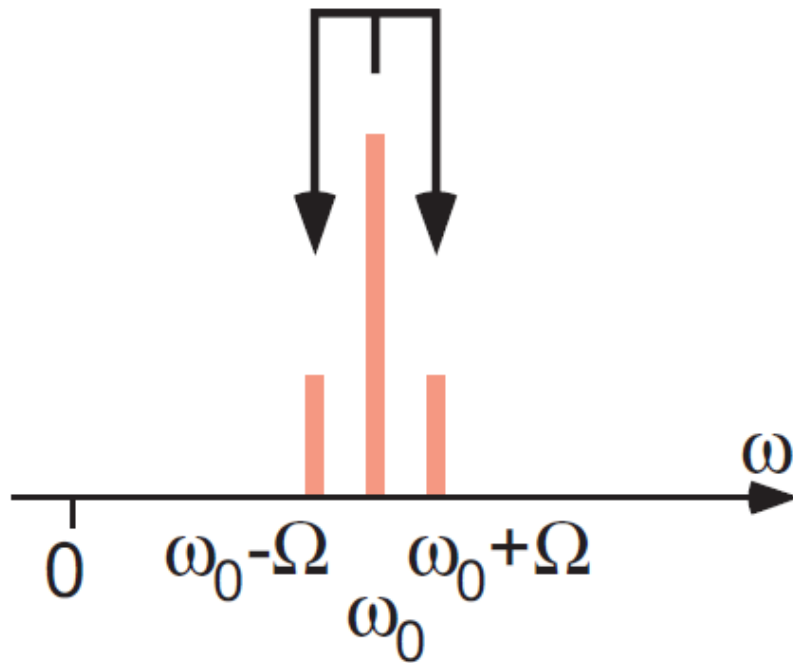


**Amplitude-to-phase  
conversion  
(free-mass)**



**Upper-to-lower  
and lower-to-upper  
conversions**

# Ponderomotive and OPO squeezings

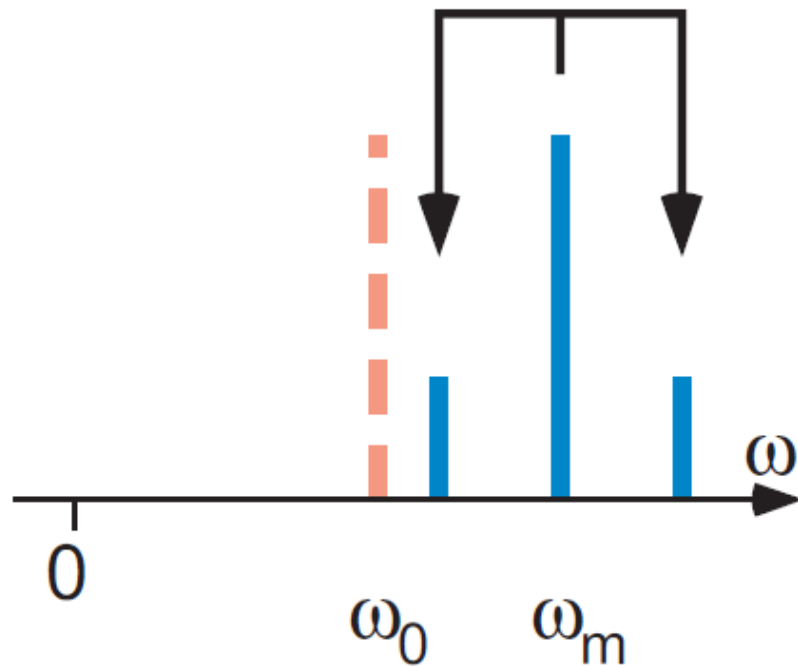


An optomechanical filter is based on this concept.

**Amplitude-to-phase  
conversion  
(free-mass)**

# Optomechanical filter

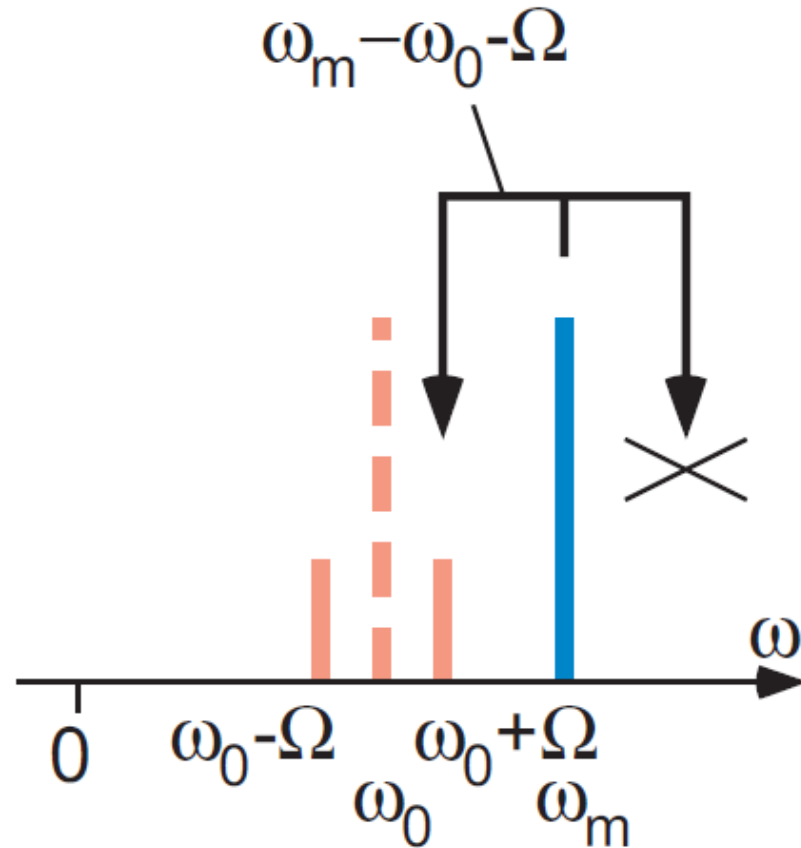
First, we shift the frequency of the beam that pumps the mechanical motion of an oscillator.



**Ponderomotive coupling  
(mechanical oscillator at  $\omega_m$ )**

# Optomechanical filter

Main signal is then injected to the system.



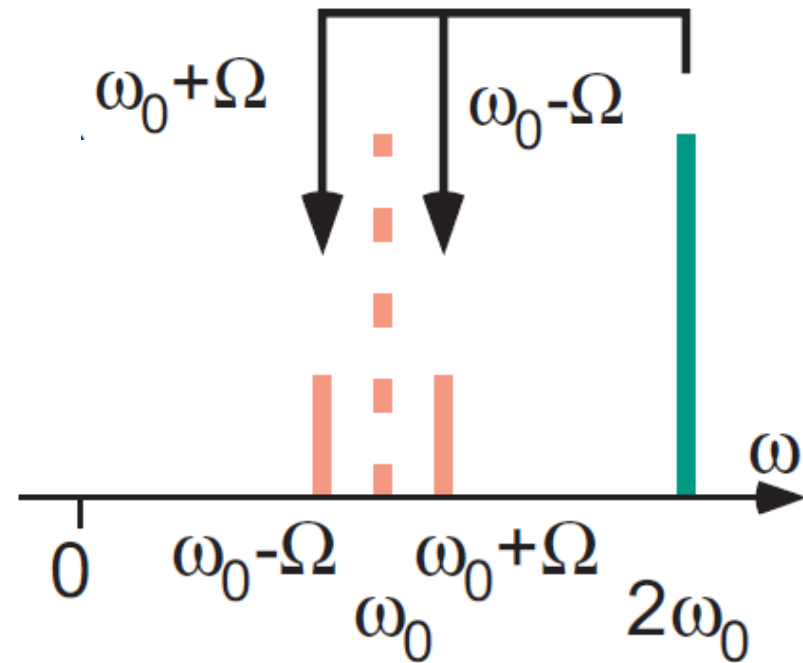
This realizes a negative dispersion of the optical field, i.e. compensation of phase delay.

**Ponderomotive coupling  
(mechanical oscillator at  $\omega_m$ )**

# Ponderomotive and OPO squeezings


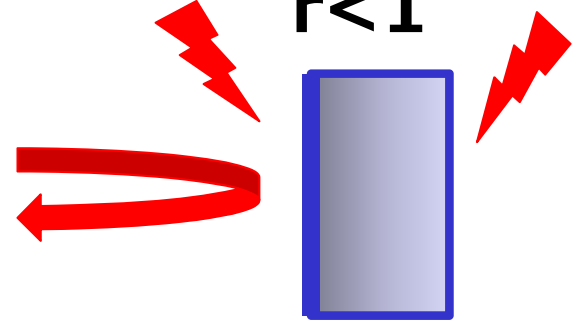




This is rather simple.  
Main signal will be increased  
("anti-squeezing").



Upper-to-lower  
and Lower-to-upper  
conversions

# Usage as a mirror

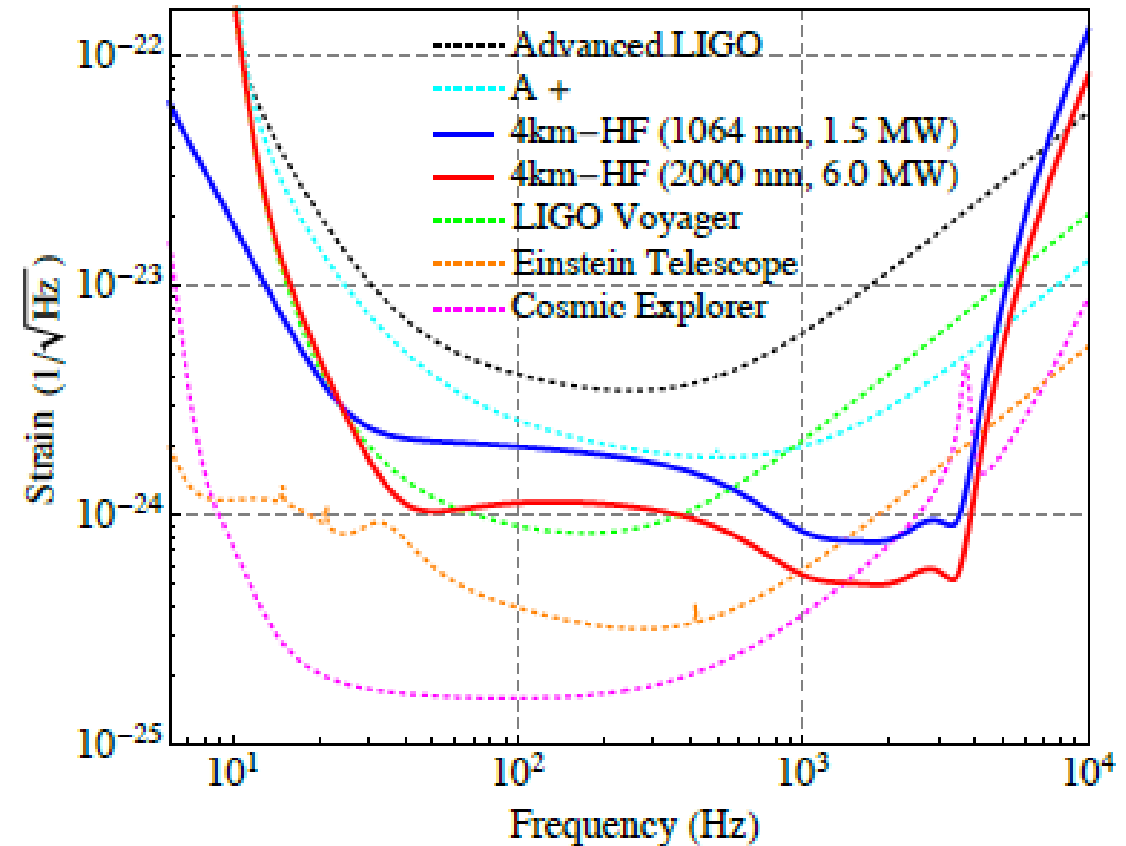
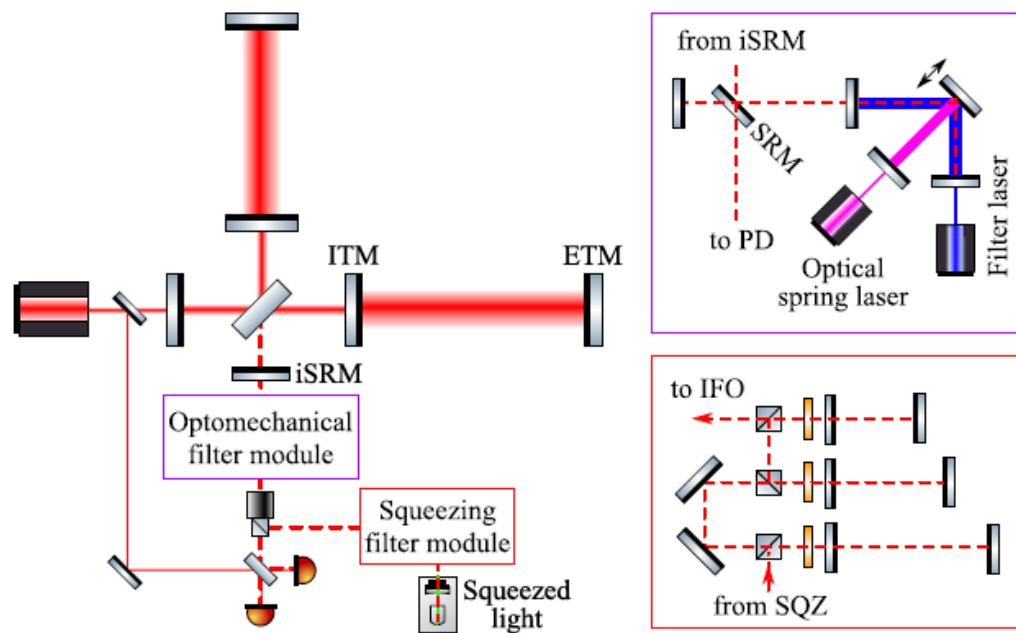
	positive	negative
gain	<p><math>r &gt; 1</math></p>  <p>Anti-lossy mirror</p>	<p><math>r &lt; 1</math></p>  <p>Lossy mirror</p>
phase	<p><math>\phi &gt; 0</math></p>  <p>Travelling with time</p>	<p><math>\phi &lt; 0</math></p>  <p>Travelling against time</p>



# Unstable optomechanical filter for bandwidth enhancement

# Current status of unstable filters

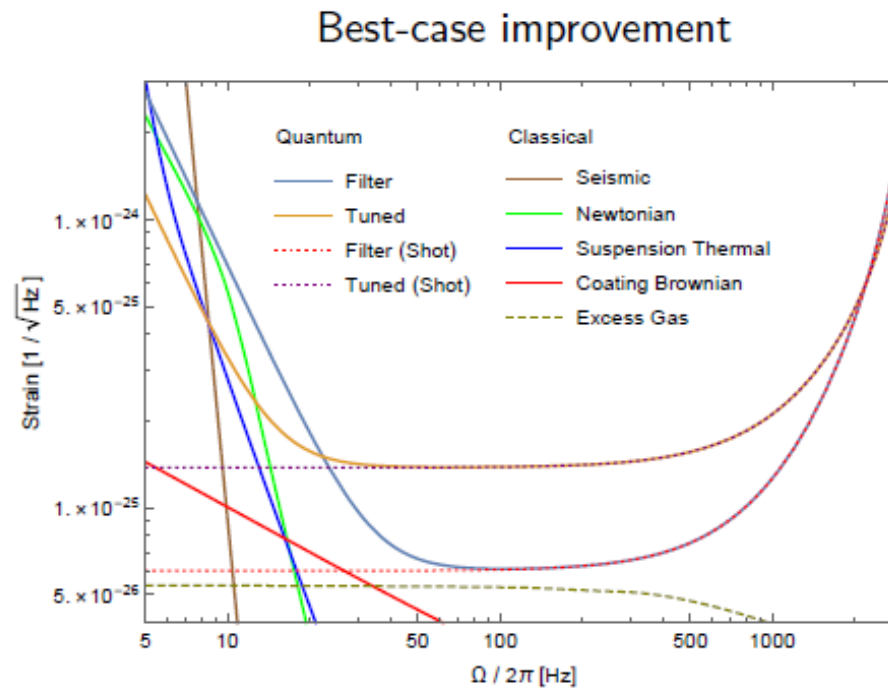
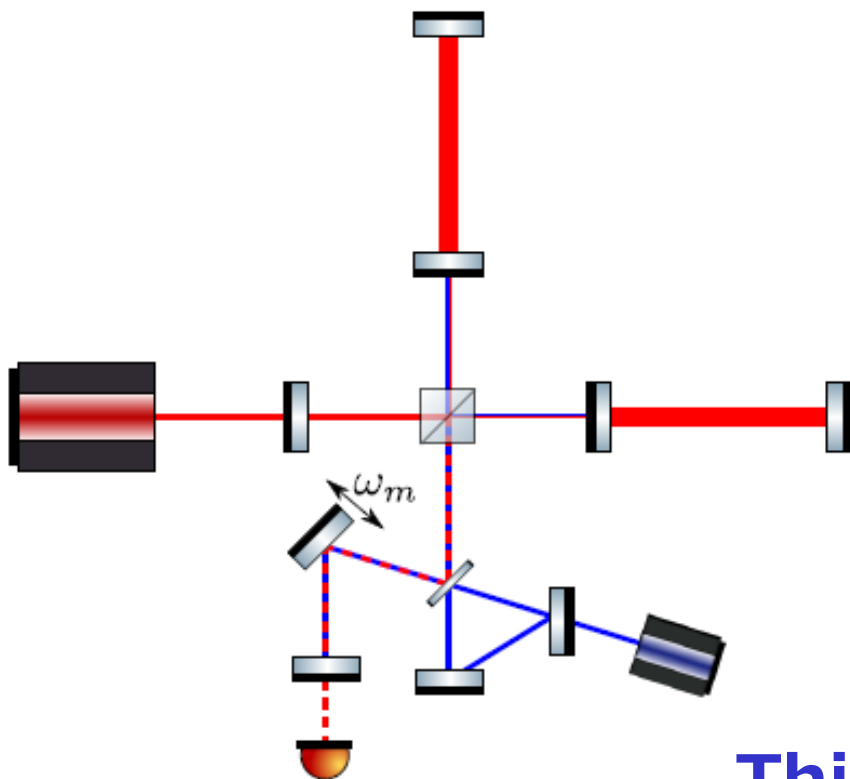
## Original design (Reflection-readout)



The design is suitable for high frequency measurements.

# Current status of unstable filters

## New design (Transmission-readout)



CE params  
 10 dB squeezing  
 $L_{\text{arm}} = 40 \text{ km}$   
 $L_{\text{SRC}} = 20 \text{ m}$   
 $T_{\text{ITM}} = 0.045$   
 $T_{\text{SRM}} = 0.00035$   
 $m_{\text{oscill.}} = 10 \text{ mg}$   
 $\omega_m = 2\pi \times 1 \text{ kHz}$   
 $P_{\text{SRC}} = 237.9 \text{ W}$

With these parameters we get  $\sim 7 \text{ dB}$  improvement  
 from 50 to 500 Hz

This design provides better sensitivity  
 at low frequencies as well and can be  
 better for long baseline detectors.

Effective BW  $\sim \frac{c}{2\sqrt{2}} \left( \frac{T_{\text{ITM}} T_{\text{SRM}}^2}{L_{\text{arm}} L_{\text{SRC}}^3} \right)^{\frac{1}{4}}$

# Current status of unstable filters

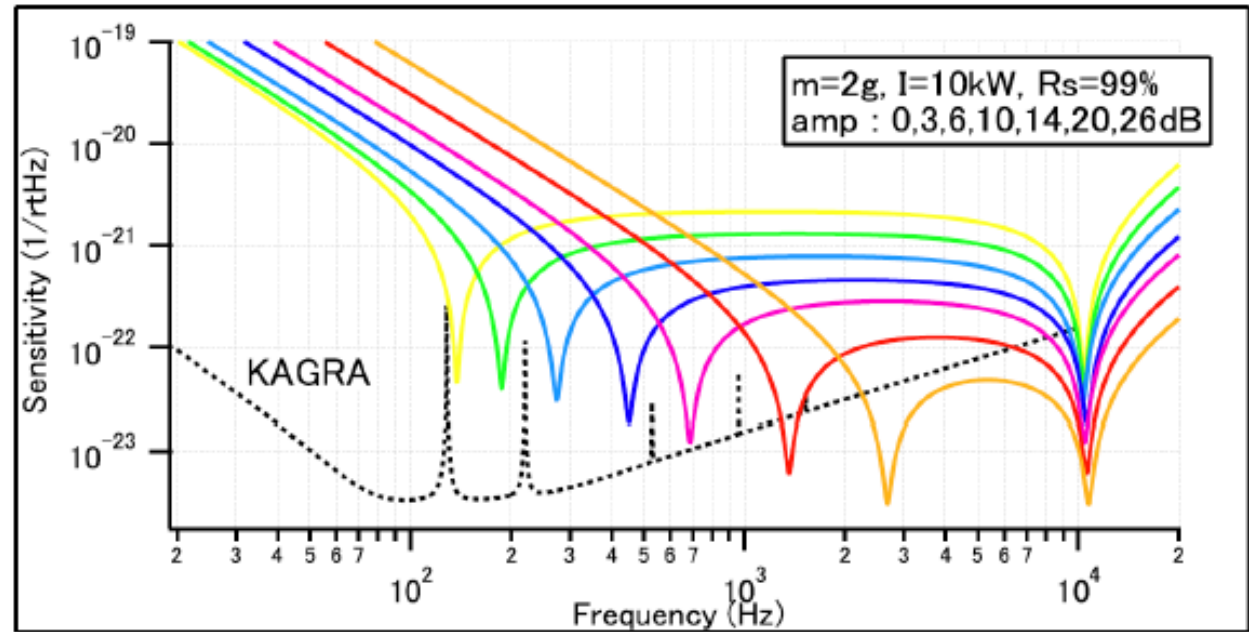
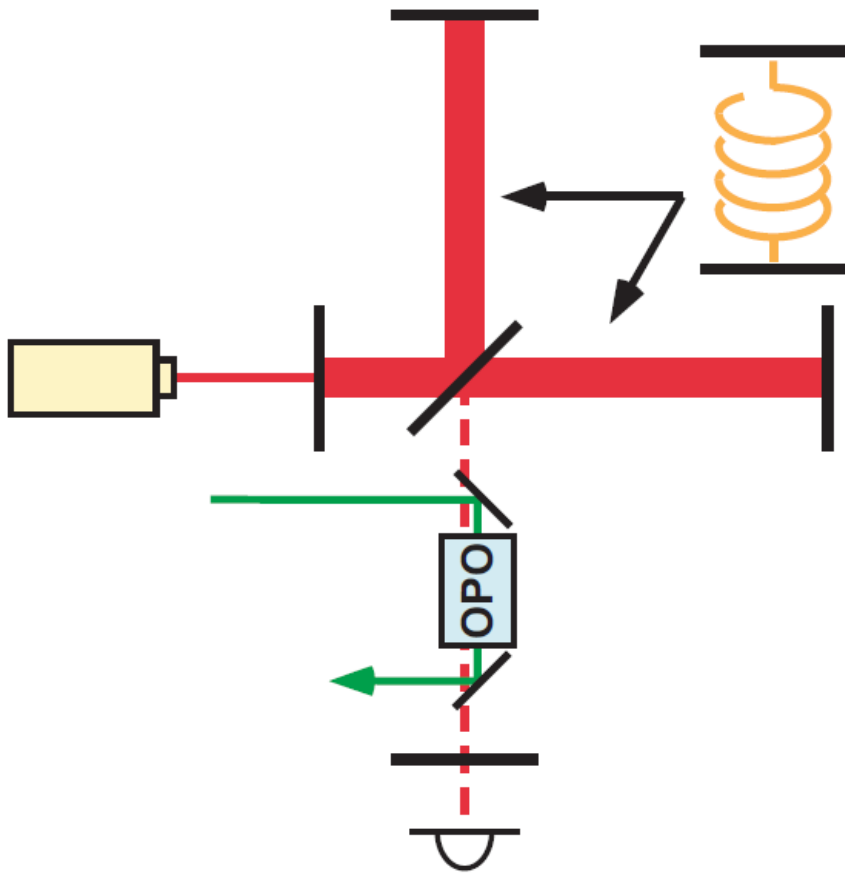
- Further to increase the BW will decrease the peak sensitivity; it can mitigate with the refl-readout
- Control of the system is an issue
- Denis Martynov is trying to realize it experimentally

## Reference

- H.Miao et al., PRL 115, 211104 (2015)
- H.Miao et al., arXiv:1712.07345 (2017)

# Intracavity OPO for signal amplification

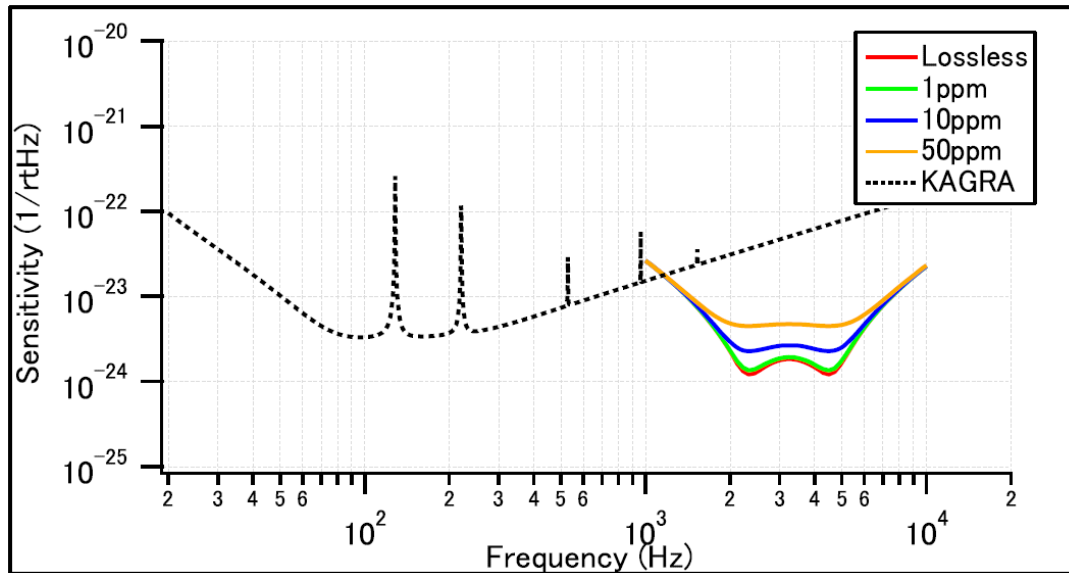
# Intracavity OPO



$$\Omega \cong \sqrt{\frac{8\omega_0 I_0}{mL^2 \gamma^2}} \frac{\sin 2\phi}{\left(r + \frac{1}{r}\right) - \left(s + \frac{1}{s}\right) \cos 2\phi}$$

The optical spring frequency increases by tuning the OPO gain to make the denominator close to zero.

# Mysteries in the current setup



This sensitivity is obtained with

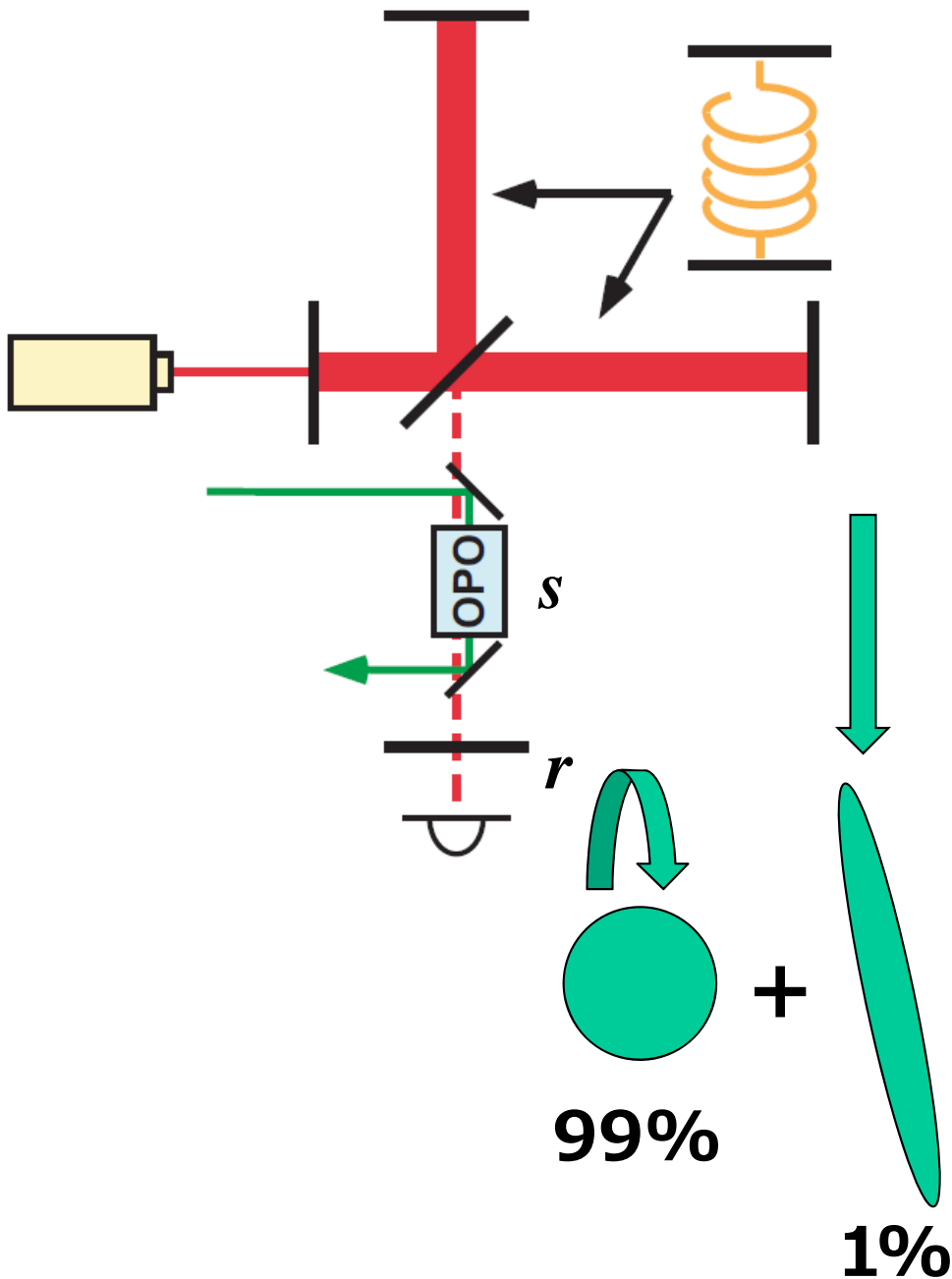
- 34dB anti-squeezing
- nearly 45 deg detuning
- no BS loss included

**I expected much smaller anti-squeezing factor and almost no contribution of the optical losses.**

**Why is the life not too easy for me?**

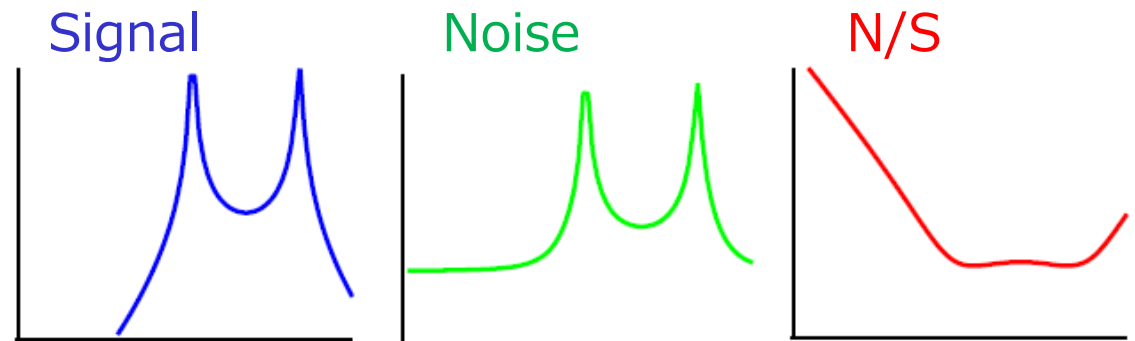


# Why 45 deg?



Both signal and noise increase in the interferometer.

However, as most of the noise field is directly reflected by SRM, the SNR can be improved by the optical spring at its resonance.



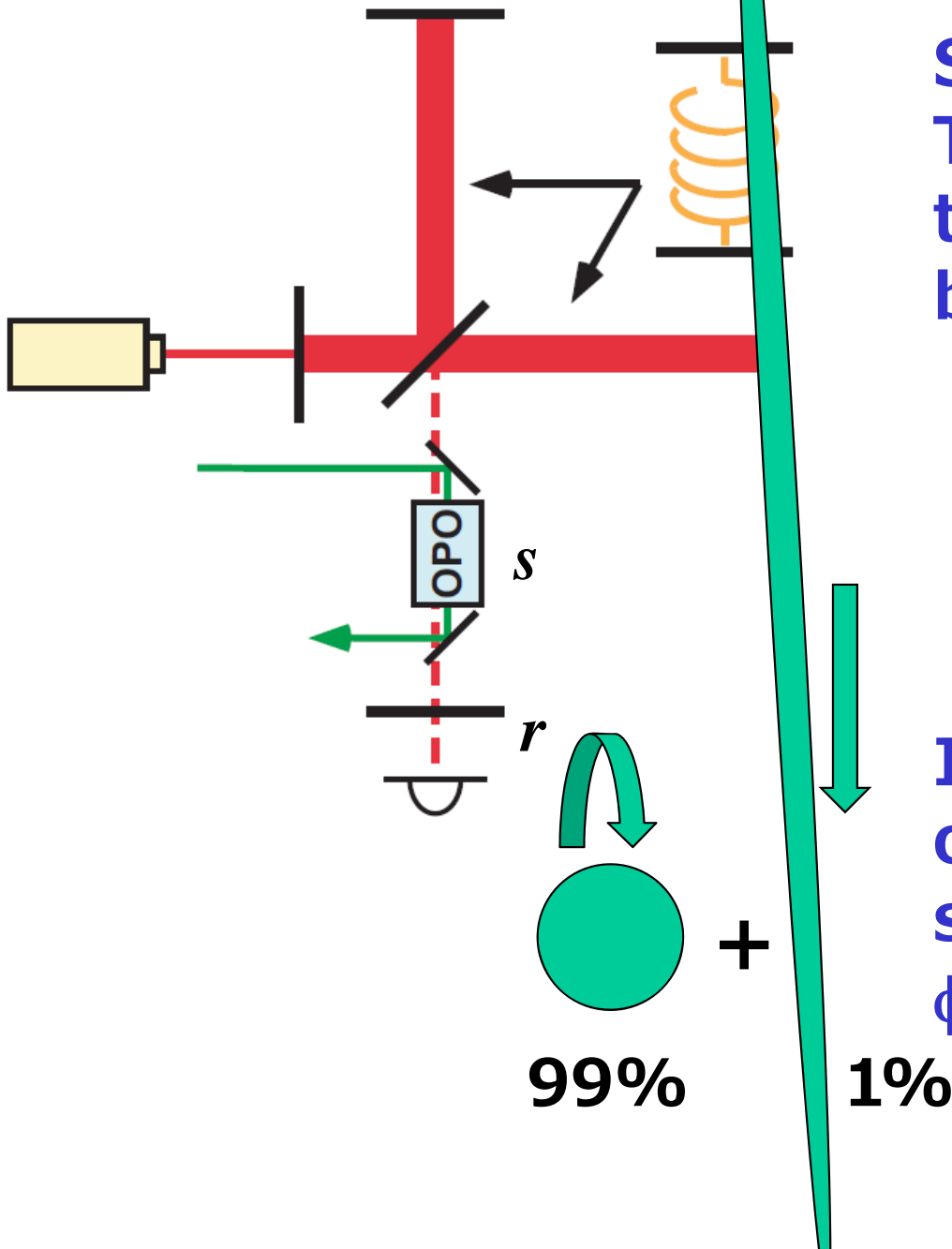


## Why 45 deg?

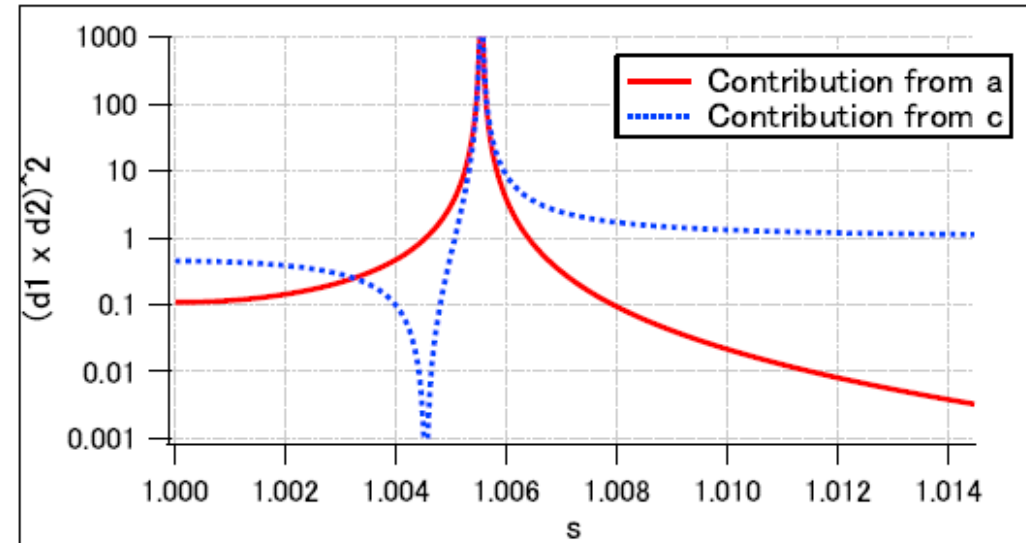
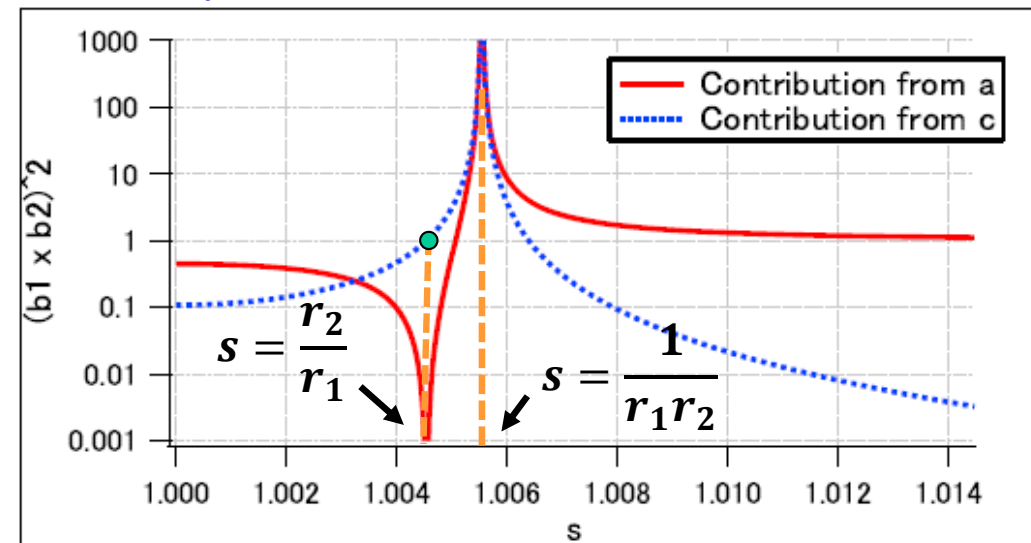
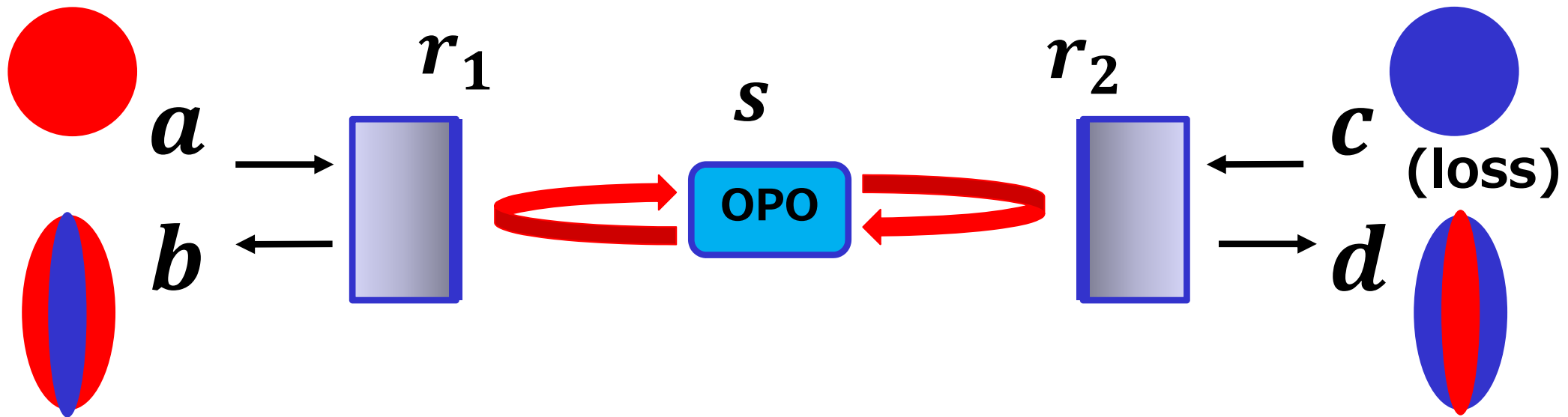
**Situation changes with an OPO.  
The intracavity gain is so high  
that the directly reflected field  
becomes negligible.**

$$\Omega \cong \sqrt{\frac{8\omega_0 I_0}{mL^2 \gamma^2} \frac{\sin 2\phi}{\left(r + \frac{1}{r}\right) - \left(s + \frac{1}{s}\right) \cos 2\phi}}$$

**It means we do not see the optical spring peak in the sensitivity spectrum, unless  $\phi$  is set to be 45 deg ( $\cos 2\phi \sim 0$ ).**



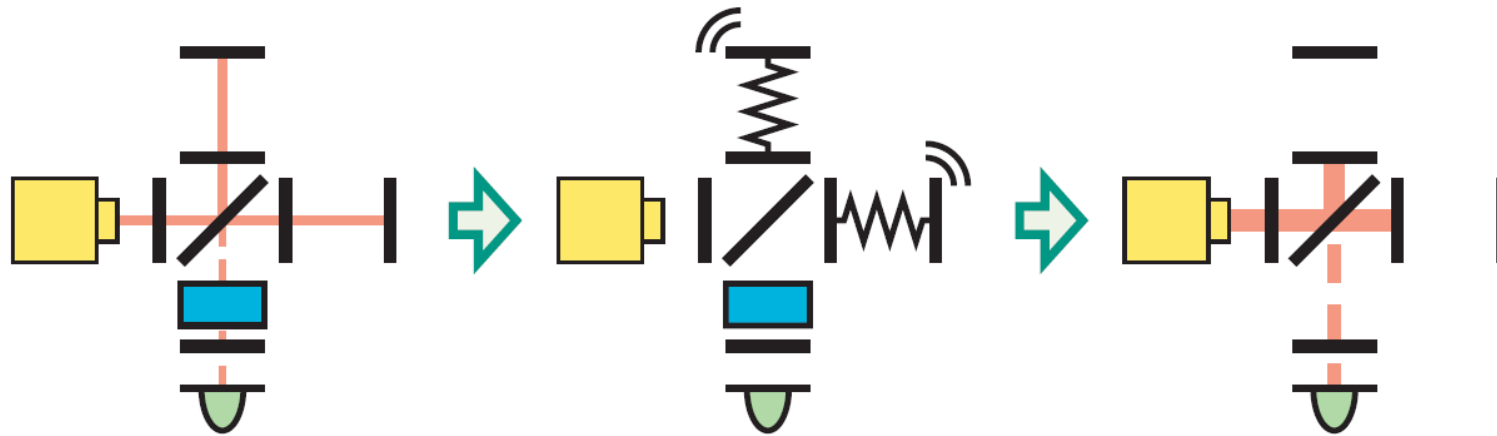
# How come the loss matters so much?



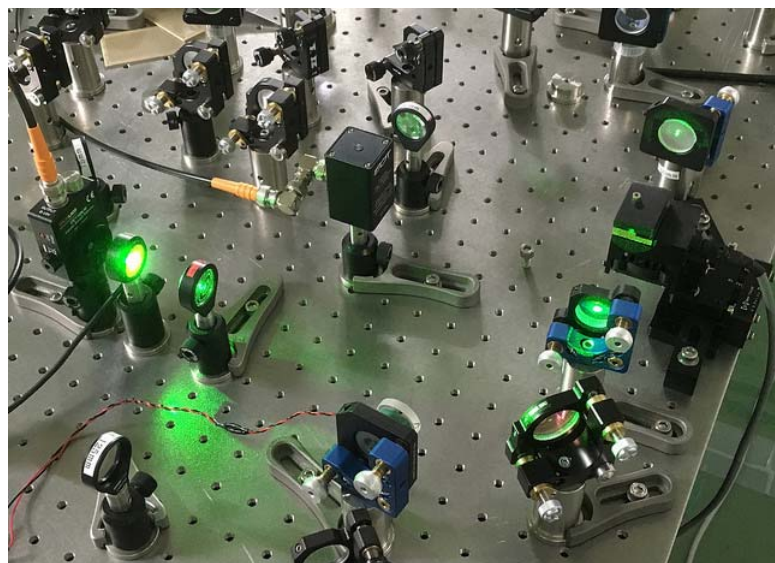
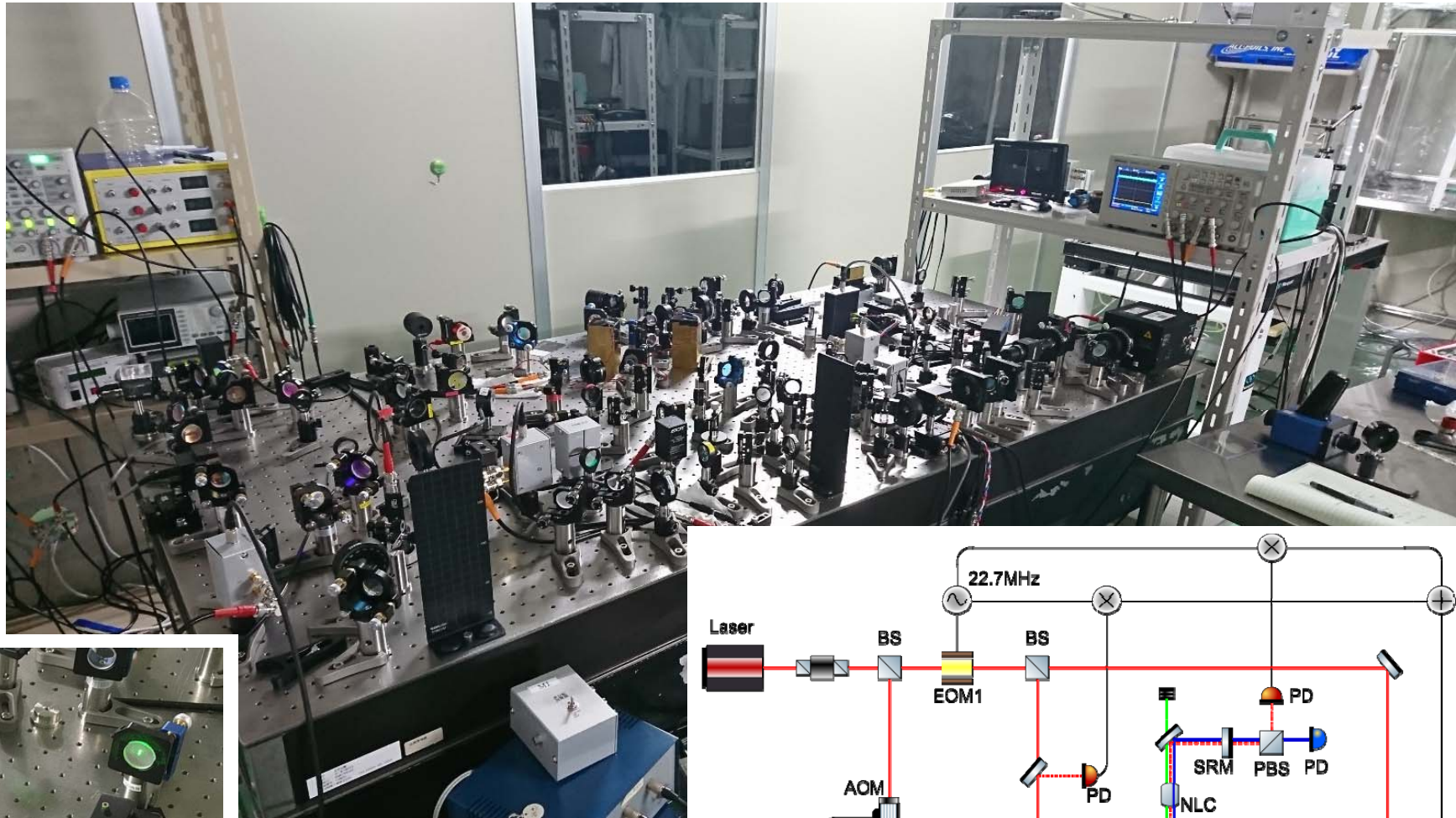
After  $s > r_2/r_1$ , the size of  $a$  in  $b$  becomes larger than unity while a coherent sum of  $a$  in  $b$  and  $d$  is still unity.

# What should we do now?

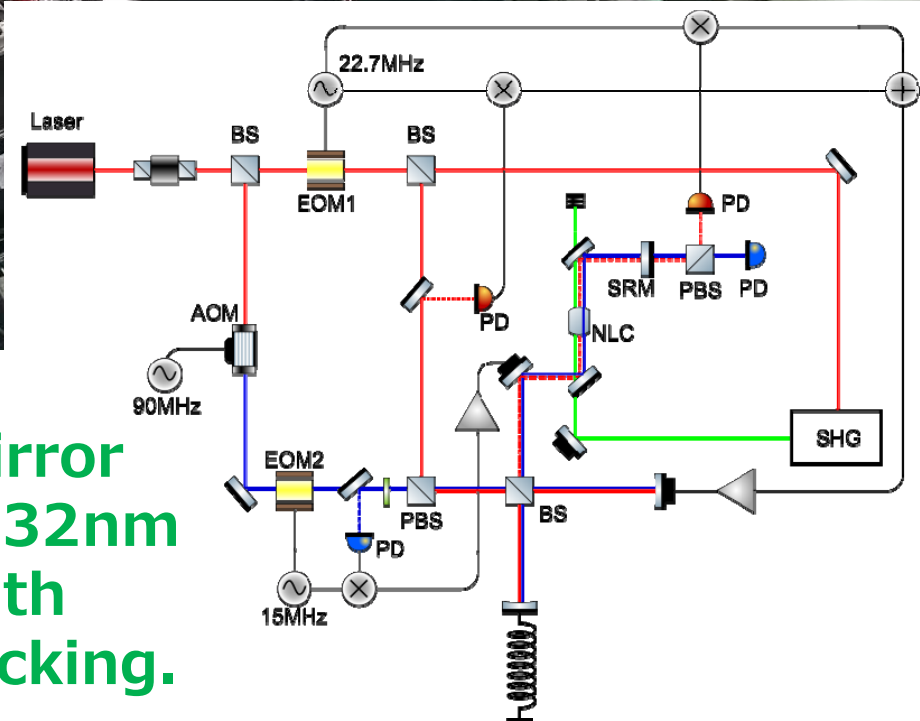
- (1) Go straight to work as planned.  
Find a low loss BS and make a high gain OPO to realize the current configuration.
- (2) Maybe we can try an *optical bar* regime.



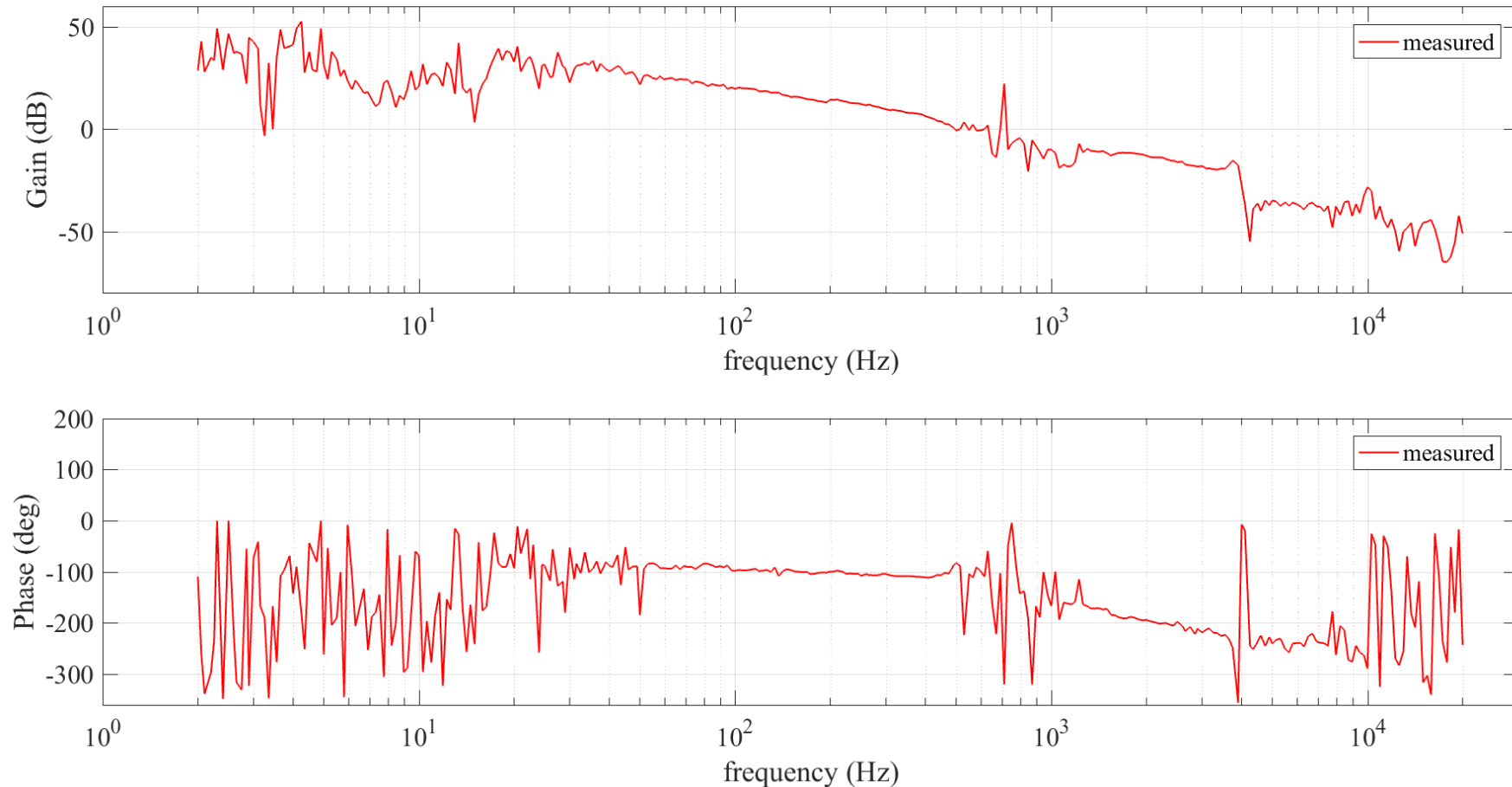
# Current status of a prototype experiment



- 200mg susp mirror
- SHG: 200mW 532nm
- Tunable SRC with a sub-carrier locking.



# Current status of a prototype experiment



- **Stable operation of detuned SRMI with an intracavity OPO**
- **No observation of optical spring yet**

# Summary

- Intracavity schemes are under development
- Control is an issue for unstable filter
- Intracavity loss mechanism has been explained
- Experimental demos are on-going/planned

# Supplementary



# Comparison

	Kentaro	Haixing
Title	Signal amplification	Negative dispersion
Goal	Optical spring at 5kHz	Bandwidth of 5kHz
Target detector	GEO-HF	aLIGO/CE
Nonlinear device	OPO	Optical spring
Challenge	Intracavity loss	Thermal noise
Stability	Marginally stable	To be controlled
Prototype	On-going	Planned